



Technology Exchange of Swirling-cutting Drill Bit and Other Downhole Tools

Jialin tian

Phone:13882236886, email:jialintian001@gmail.com

Southwest petroleum university

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1、旋切钻头

结合前期研究成果，主要说明旋切钻头关键参数轮体速比、轮体夹角 β 轴颈偏移量 s ，对井底模型的影响。

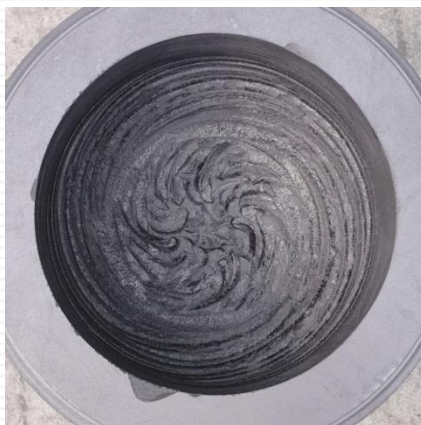
2.1 井底模型关键参数影响分析

2.1.1 研究基础

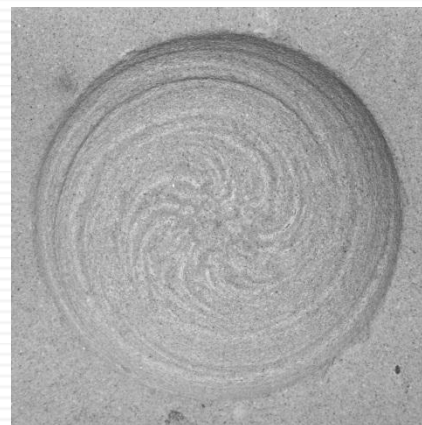
(一) 建立旋切钻头前期研究成果总结，完成相关研究



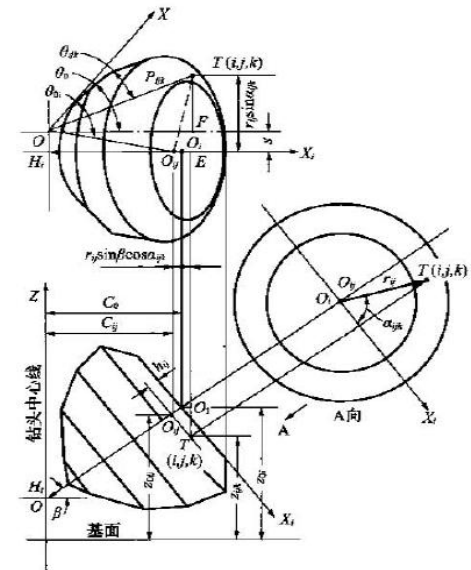
实验钻进



反转 (s 为负值, 顺时针旋风)



正转 (s 为正值, 逆时针旋风)



运动轨迹方程

$$\begin{aligned}\rho_Q &= \sqrt{(C_0 - h_Q \cos \beta + r_Q \sin \beta \cos \alpha_Q)^2 + (r_Q \sin \alpha_Q - s)^2} \\ \theta_Q &= \theta_0 - \frac{2\pi(i-1)}{3} - \tan^{-1}\left(\frac{r_Q \sin \alpha_Q - s}{C_0 - h_Q \cos \beta + r_Q \sin \beta \cos \alpha_Q}\right) \\ z_Q &= z_Q - h_Q \sin \beta - r_Q \cos \beta \cos \alpha_Q\end{aligned}$$

速度方程

$$v_{Q\rho} = \frac{d\rho_Q}{dt} = \lambda_{Q\rho} r_Q \omega_i$$

$$v_{Qt} = \rho_Q \frac{d\theta_Q}{dt} = \rho_Q \omega_b - \lambda_{Qt} r_Q \omega_i$$

$$v_{Qz} = \frac{dz_Q}{dt} = v_{bz} + \lambda_{Qz} r_Q \omega_i$$

$$\lambda_{Q\rho} = \frac{\left[\frac{r_Q}{2} \cos^2 \beta \sin 2\alpha_Q - (C_0 - h_Q \cos \beta) \sin \beta \sin \alpha_Q - s \cos \alpha_Q \right]}{\sqrt{(C_0 - h_Q \cos \beta + r_Q \sin \beta \cos \alpha_Q)^2 + (r_Q \sin \alpha_Q - s)^2}}$$

$$\lambda_{Qt} = \frac{(C_0 - h_Q \cos \beta) \cos \alpha_Q + r_Q \sin \beta - s \sin \beta \sin \alpha_Q}{\rho_Q^2}$$

$$\lambda_{Qz} = \cos \beta \sin \alpha_Q$$

$$a_{Q\rho} = \frac{r_Q}{\rho_Q} \left[\frac{r_Q}{2} \cos^2 \beta \sin 2\alpha_Q - (C_0 - h_Q \cos \beta) \sin \beta \sin \alpha_Q - s \cos \alpha_Q \right] \varepsilon_c$$

$$+ \frac{r_Q}{\rho_Q} \left[r_Q \cos^2 \beta \cos 2\alpha_Q - (C_0 - h_Q \cos \beta) \sin \beta \sin \alpha_Q + s \sin \alpha_Q \right] \omega_c^2$$

$$- \frac{r_Q}{\rho_Q^3} \left[\frac{r_Q}{2} \cos^2 \beta \sin 2\alpha_Q - (C_0 - h_Q \cos \beta) \sin \beta \sin \alpha_Q - s \sin \alpha_Q \right]^2 \omega_c^2$$

$$- \rho_Q (\omega_b - \lambda_{Qt} r_Q \omega_i)^2$$

$$a_{Qt} = \rho_Q [\varepsilon_b - m \varepsilon_c - (m)' \omega_c^2] + 2(\omega_b - \lambda_{Qt} r_Q \omega_i) r_Q \lambda_{Q\rho} \omega_i$$

$$a_{Qz} = a_{oz} + r_Q \cos \beta \cos \alpha_Q \varepsilon_c + r_Q \cos \beta \cos \alpha_Q \omega_c^2$$

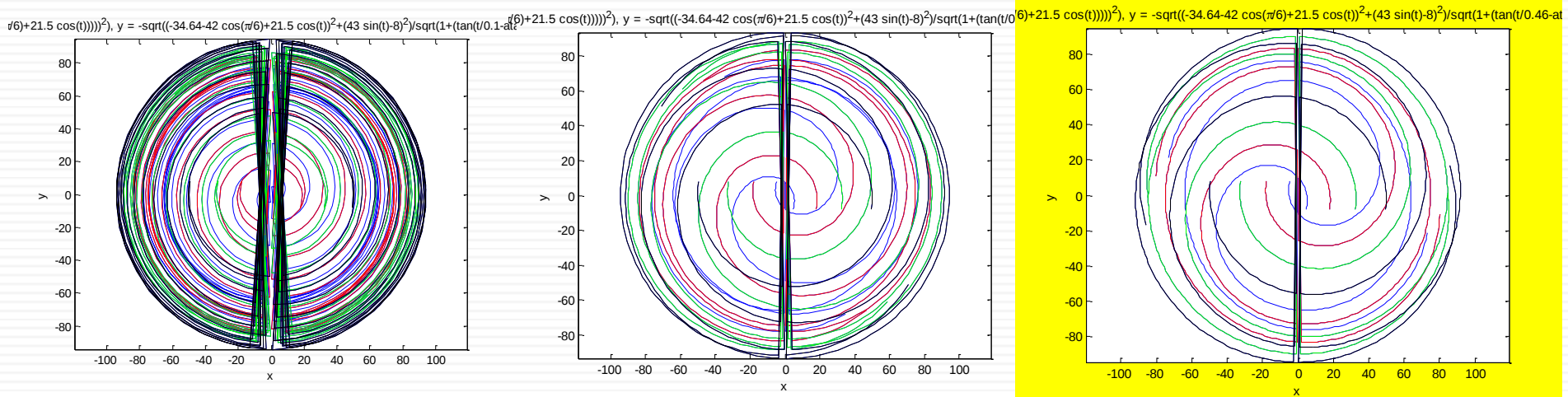
$$m = r_Q [(C_0 - h_Q \cos \beta) \cos \alpha_Q + r_Q \sin \beta - s \sin \beta \sin \alpha_Q] / [(C_0 - h_Q \cos \beta + r_Q \sin \beta \cos \alpha_Q)^2 + (r_Q \sin \alpha_Q - s)^2]$$

$$(m)' = \frac{-r_Q [(C_0 - h_Q \cos \beta) \cos \alpha_Q \sin \alpha_Q - s \sin \beta \cos \alpha_Q]}{(C_0 - h_Q \cos \beta + r_Q \sin \beta \cos \alpha_Q)^2 + (r_Q \sin \alpha_Q - s)^2}$$

$$- \{r_Q^2 [(C_0 - h_Q \cos \beta) \cos \alpha_Q - s \sin \beta \sin \alpha_Q + r_Q \sin \beta] [r_Q \cos^2 \beta \sin 2\alpha_Q$$

$$- 2(C_0 - h_Q \cos \beta) \sin \beta \sin \alpha_Q - 2s \cos \alpha_Q]\} / [(C_0 - h_Q \cos \beta + r_Q \sin \beta \cos \alpha_Q)^2 + (r_Q \sin \alpha_Q - s)^2]^2$$

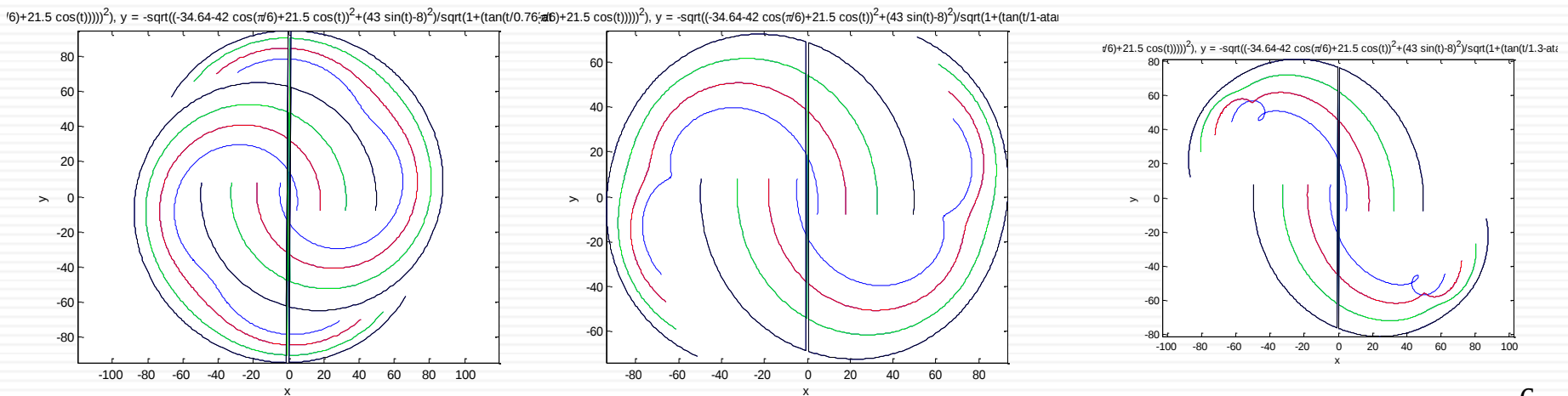
2.1.2 轮体速比对井底模型的影响



轮体速比=0.1

轮体速比=0.3

轮体速比=0.46



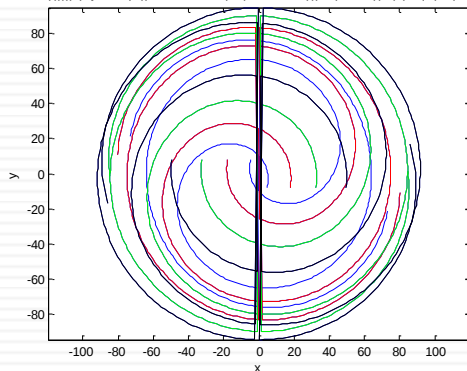
轮体速比=0.76

轮体速比=1

轮体速比=1.3

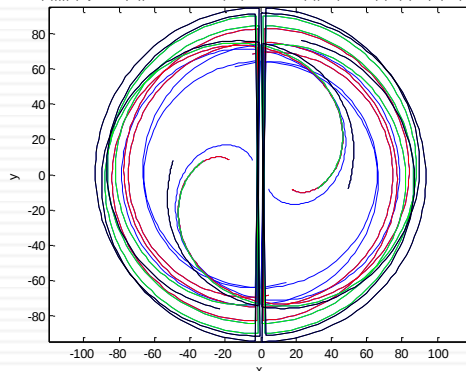
2.1.3 轴颈偏移量（含齿轮转向布置）对井底模型的影响

$$y = \sqrt{(-34.64 - 42 \cos(\pi/6) + 21.5 \cos(t))^2 + (43 \sin(t) - 8)^2} / \sqrt{1 + (\tan(t/0.46 - \pi/6))^2}$$



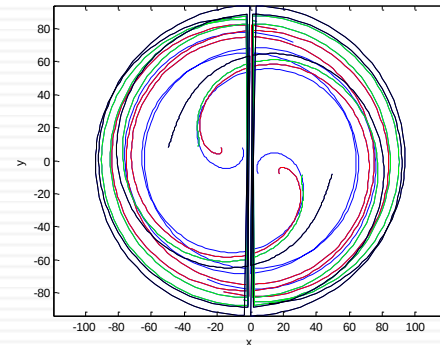
钻头正向，齿轮正向

$$y = \sqrt{(-34.64 - 42 \cos(\pi/6) + 21.5 \cos(-t))^2 + (43 \sin(-t) - 8)^2} / \sqrt{1 + (\tan(t/0.46 - \pi/6))^2}$$



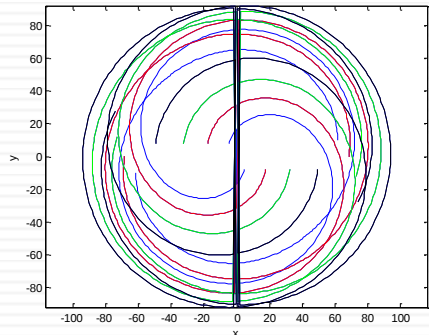
钻头正向，齿轮负向

$$y = \sqrt{(-34.64 - 42 \cos(\pi/6) + 21.5 \cos(t))^2 + (43 \sin(t) + 8)^2} / \sqrt{1 + (\tan(t/0.46 - \pi/6))^2}$$



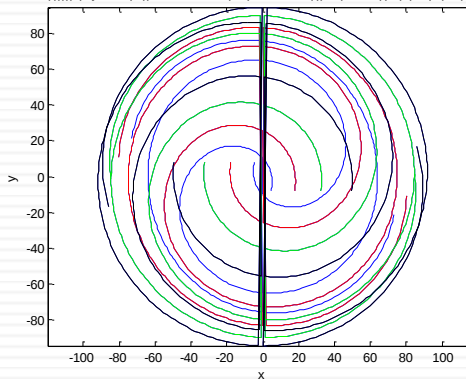
钻头负向，齿轮正向

$$y = \sqrt{(-34.64 - 42 \cos(\pi/6) + 21.5 \cos(-t))^2 + (43 \sin(-t) - 8)^2} / \sqrt{1 + (\tan(t/0.46 - \pi/6))^2}$$



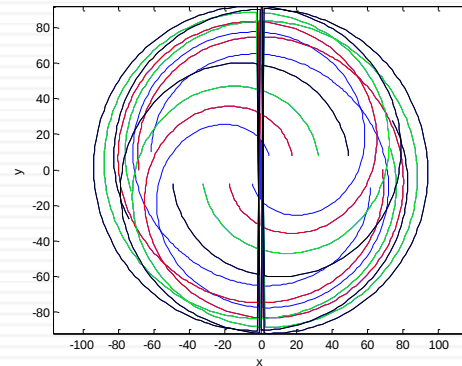
钻头负向，齿轮负向

$$y = \sqrt{(-34.64 - 42 \cos(\pi/6) + 21.5 \cos(t))^2 + (43 \sin(t) - 8)^2} / \sqrt{1 + (\tan(t/0.46 - \pi/6))^2}$$



S=+8MM

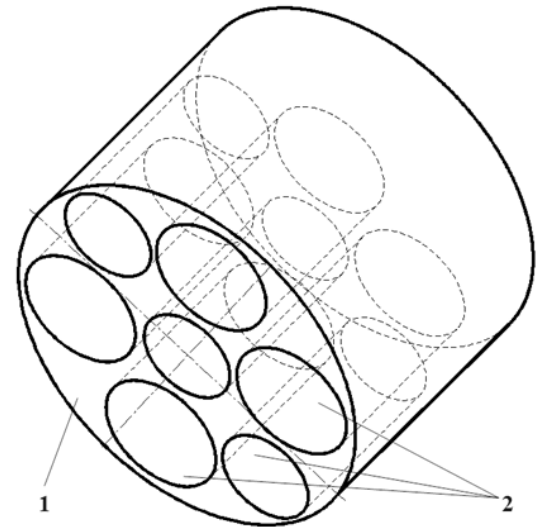
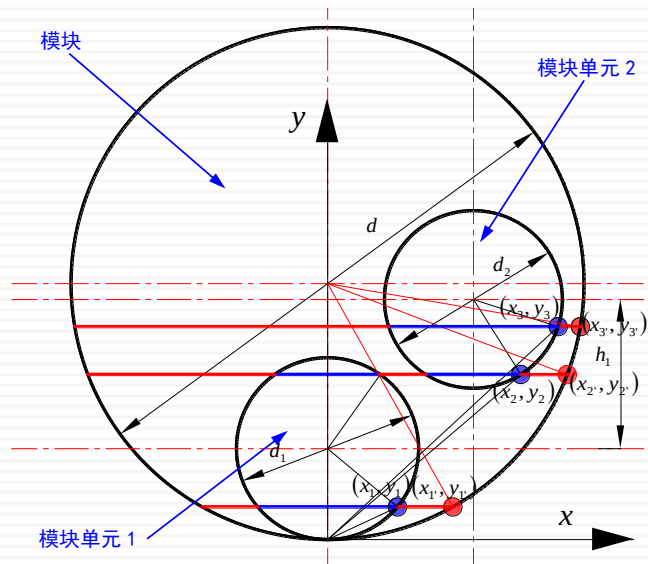
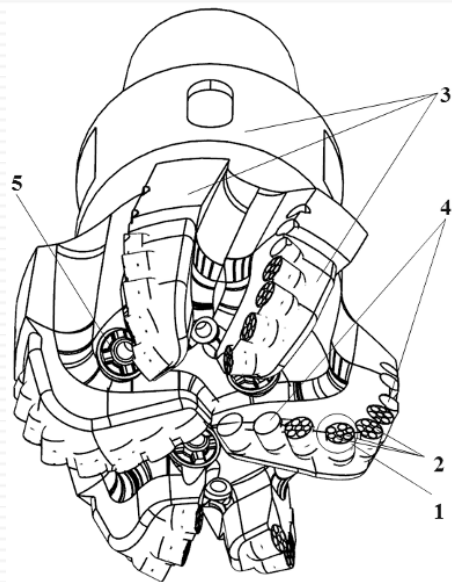
$$y = \sqrt{(-34.64 - 42 \cos(\pi/6) + 21.5 \cos(t))^2 + (43 \sin(t) + 8)^2} / \sqrt{1 + (\tan(t/0.46 - \pi/6))^2}$$



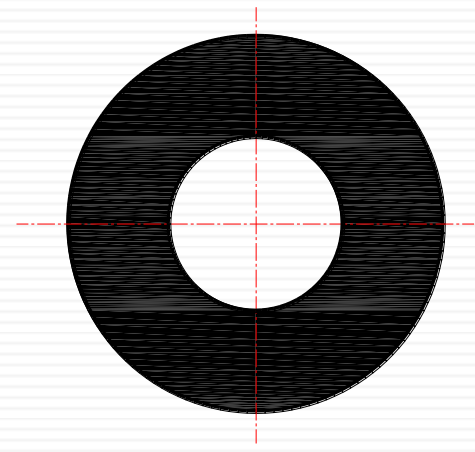
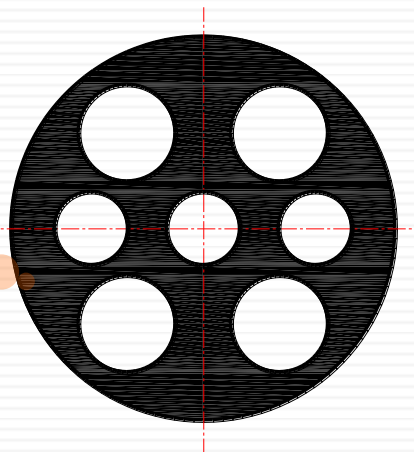
S=-8MM

2.2 模块PDC

根据前期研究结果，对后期的思考



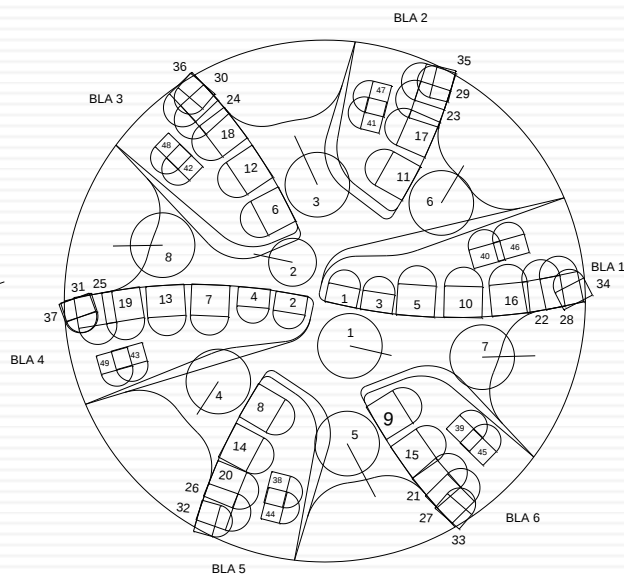
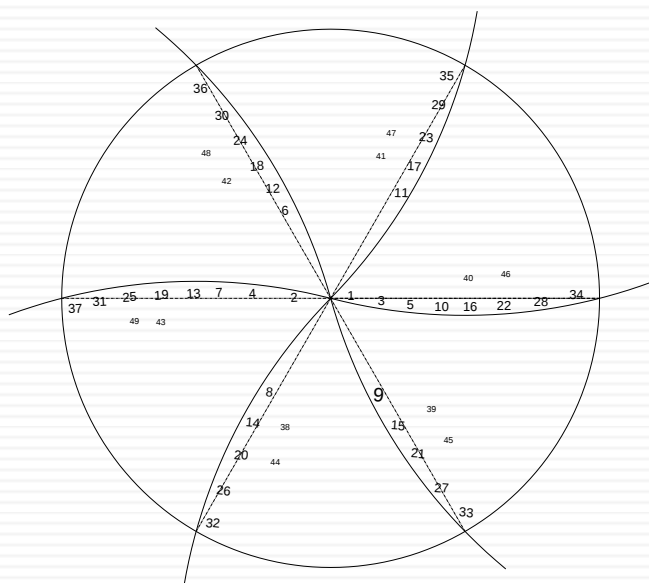
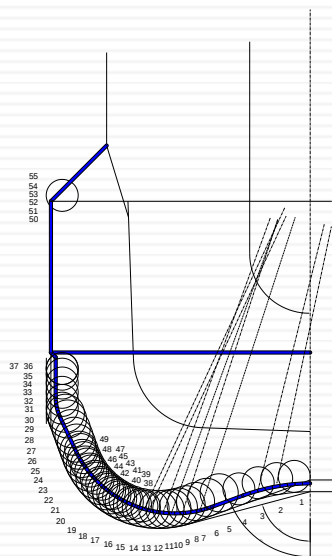
另一种补充
(挖空)?



2.3 PDC布齿基础研究

现场反馈问题：（供参考）PDC中心齿的倾斜角，对齿的覆盖率、干涉、破岩率的影响，PDC的基础问题。编软件进行科学设计？

失效部位(中心、外围、保径)、失效形式（磨损、冲击、磨损）？



2、螺杆钻具（PDM）



橡胶性能、温度等基本参数对橡胶配合过盈量、钻具寿命的影响？

（一）、常规衬套与等壁厚衬套计算结果

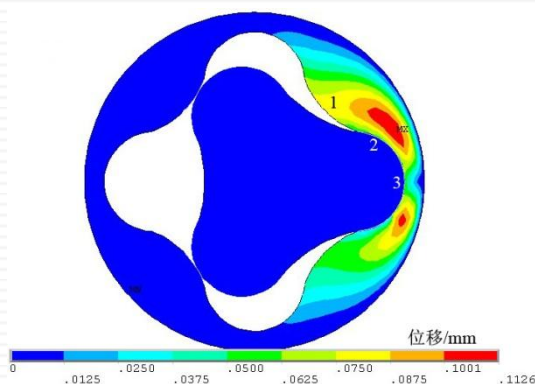


图1 10MPa内压常规衬套位移云图

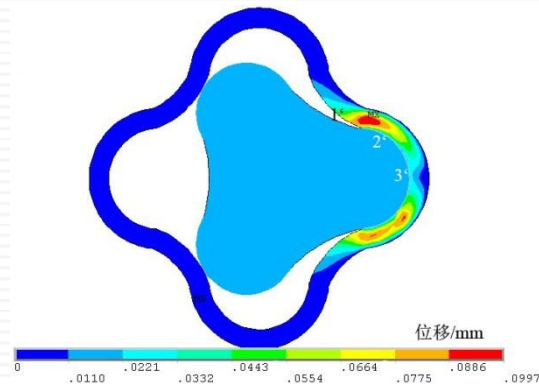


图2 10MPa内压等壁厚衬套位移云图

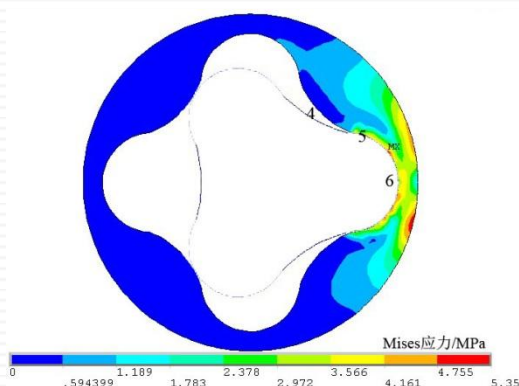


图3 10MPa内压常规衬套Mises应力云图

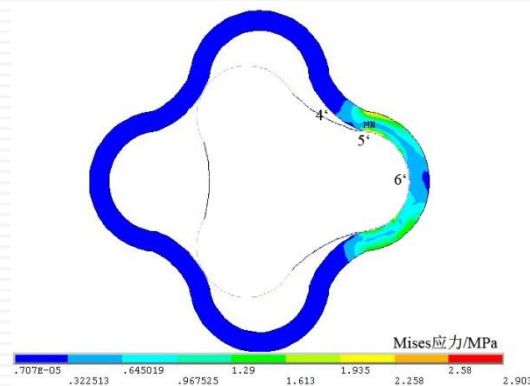
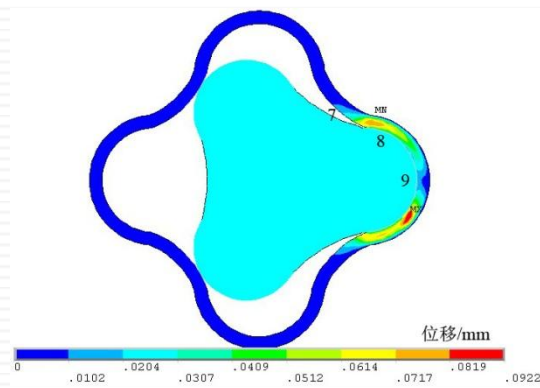
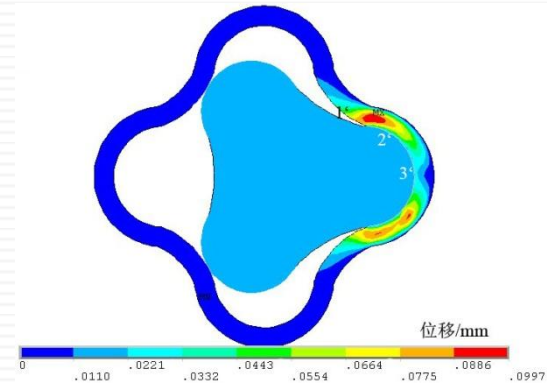


图4 10MPa内压等壁厚衬套Mises应力云图

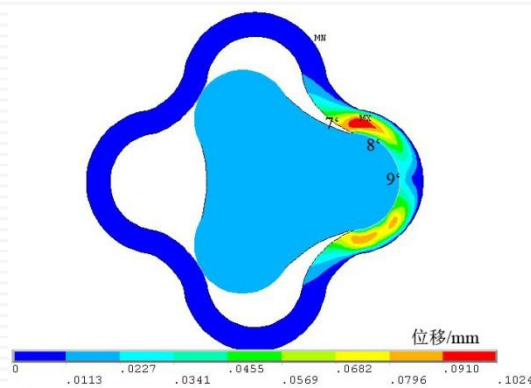
(二)、厚度变化对衬套性能影响



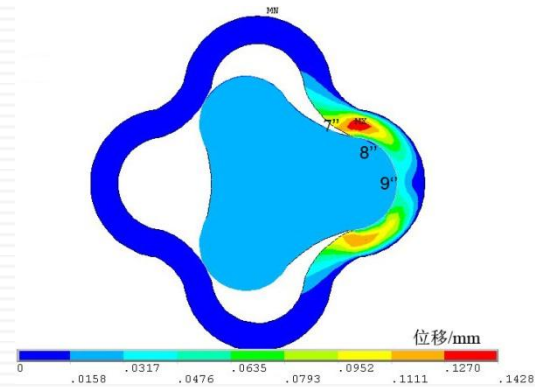
厚度5mm等壁厚衬套位移云图



厚度8mm等壁厚衬套位移云图



厚度10mm等壁厚衬套位移云图



厚度12mm等壁厚衬套位移云图

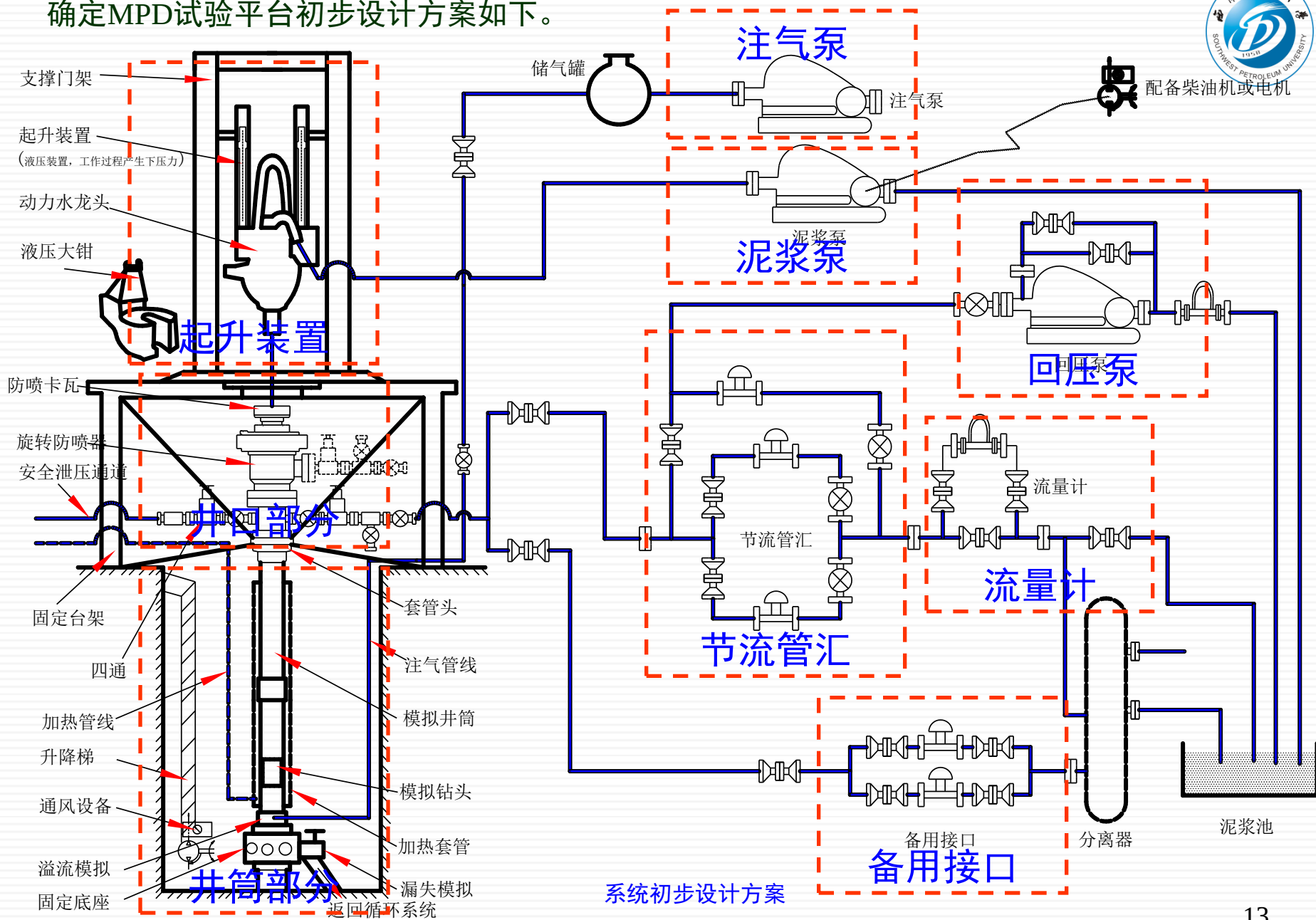
3、其他井下工具



3.1 钻井新工艺

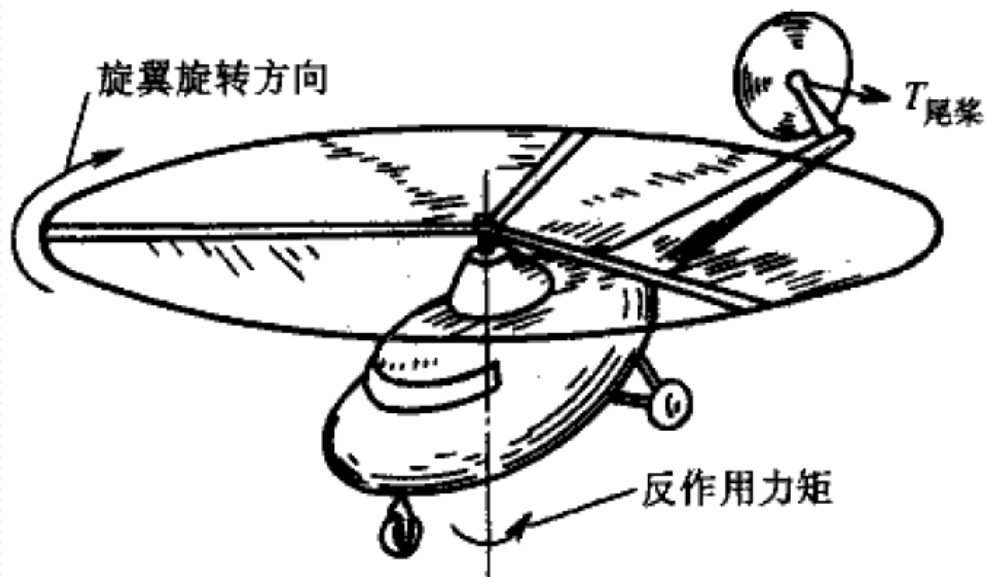
- (1) 连续循环钻井
- (2) 高温钻井在非开挖中的应用
- (3) MPD钻井?

确定MPD试验平台初步设计方案如下。

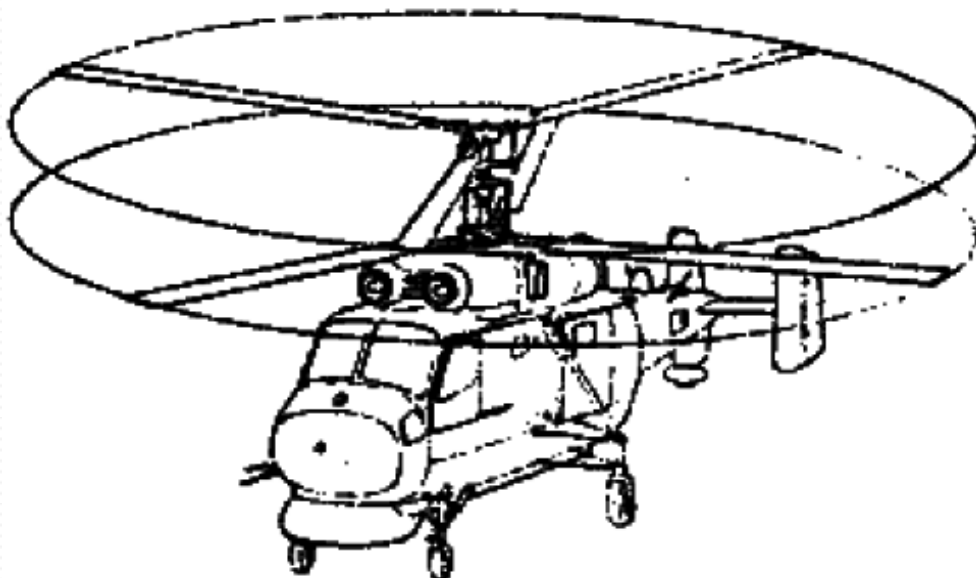


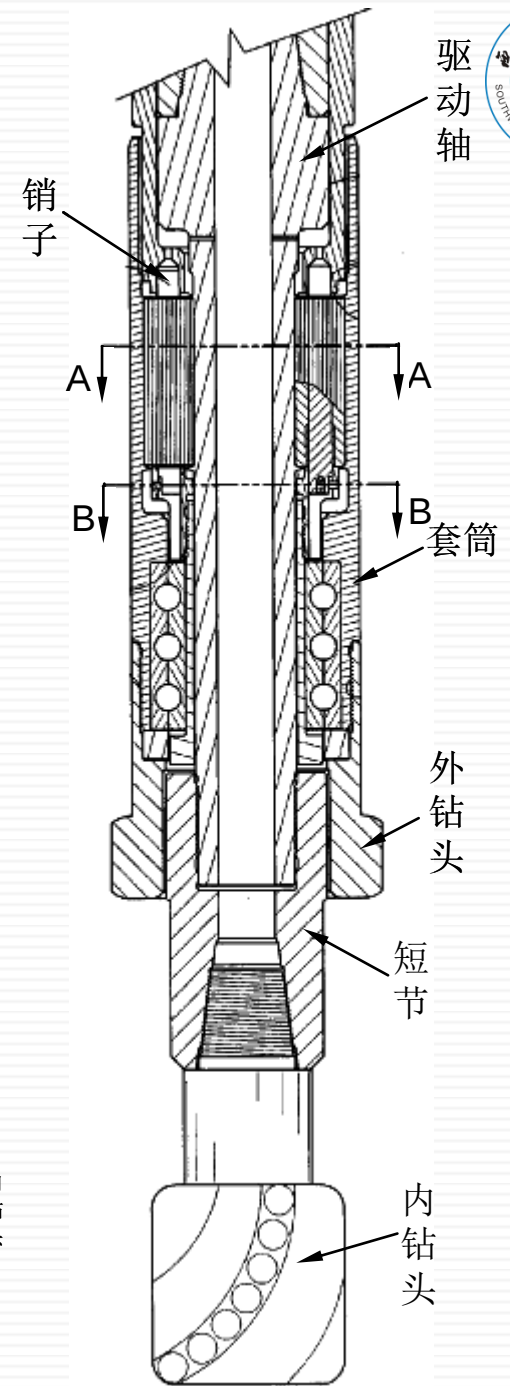
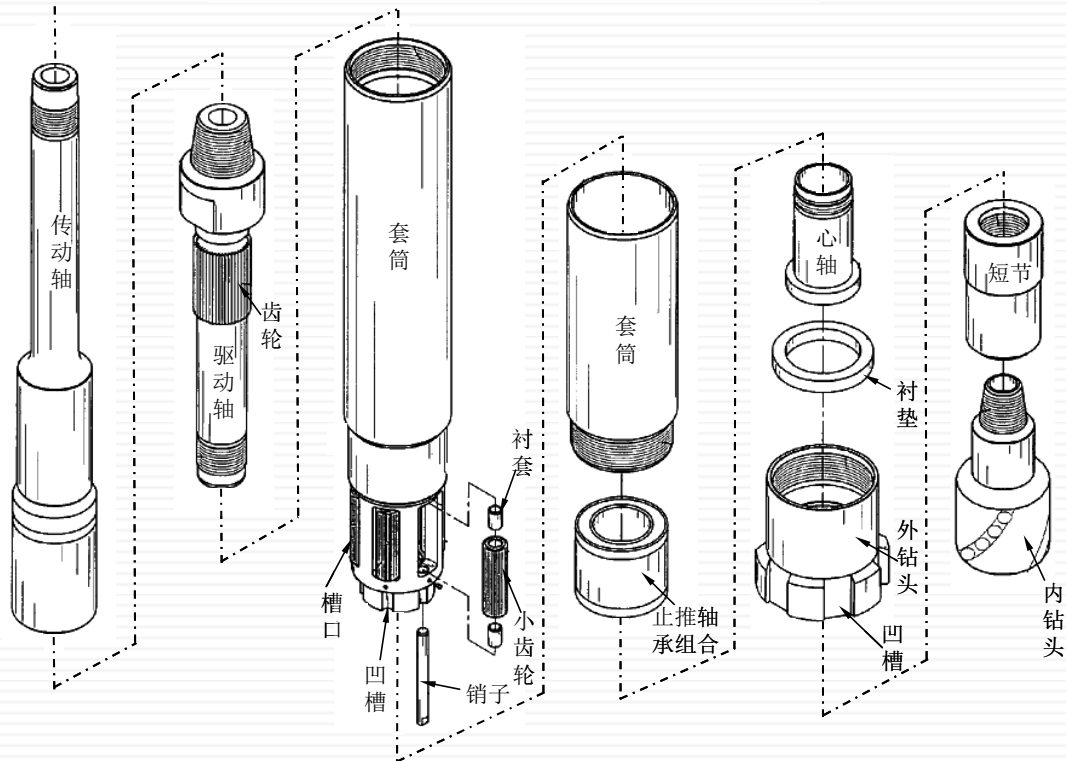
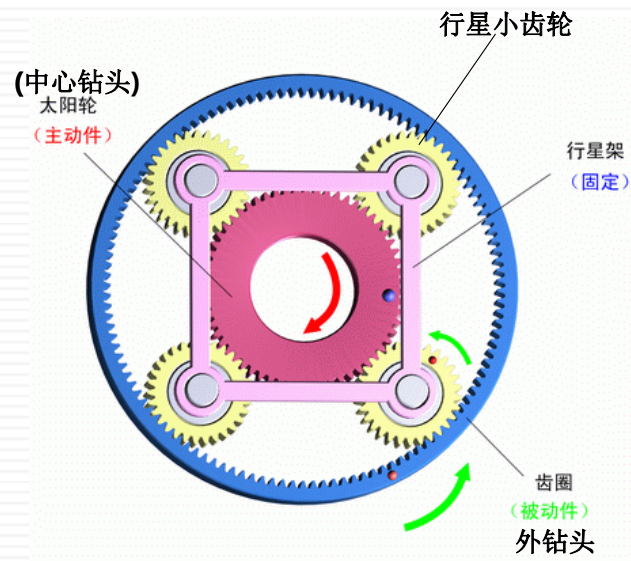
(3) 一种新型无反扭矩的钻具

单旋翼直升机的反扭矩



共轴双旋翼直升机





谢谢！

